

RESEARCH ARTICLE

ON MODEL OF SHIP MOVEMENT CONTROL WITH ACCOUNT POSSIBILITY OF CHANGING OF MASS OF CARGO

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ABSTRACT

In this paper we presents a model of vessel motion control with the possibility to change the cargo mass. In the framework of the model we consider external forces acting on the vessel, the magnitude of which can be variable. We also present an analyti-cal approach for analysis of the considered model. The approach gives a possibility to take into account changing of parameters of the in time, as well as the nonlinearity of the model.

Keywords: vessel motion control; control model; analytical approach for analysis.

INTRODUCTION

Vessel controllability is a topical issue to decrease quantity of accidents and optimizing cargo transportation. In this regard, a forecast of vessel movement is necessary. One of the classic methods for choosing a vessel's route is to calculate its possible trajectory depending on various parameters [1-5]. Another topical issue is increasing the buoyancy and stability of a vessel. In this paper we intro-duce a vessel movement model that is more general than those introduced in liter-ature. We also presents an analytical approach to analyze the model

METHODOLOGY

Motion of a vessel can be described on the basis of Newton's second law [1-7]. In the framework of this law, changing of the projections of the corresponding velocities is described by the following equations

$$\begin{aligned} (m + m_x) \frac{d v_x}{d t} &= F_{x1} + F_{x2}; (L_{xx} + L_x) \frac{d \omega_x}{d t} = M_{kr} - \rho g V x_1 + \sum_{n=1}^N P_n x_{2n} + M_{x1} + M_{x2} \\ (m + m_y) \frac{d v_y}{d t} &= F_{y1} + F_{y2}; (L_{yy} + L_y) \frac{d \omega_y}{d t} = M_{diff} - \rho g V y_1 + \sum_{n=1}^N P_n y_{2n} + M_{y1} + M_{y2} \end{aligned} \quad (1)$$

$$(m + m_z) \frac{d v_z}{d t} = \rho g V - F_g - \sum_{n=1}^N P_n + F_{z1} + F_{z2};$$

$$(L_{zz} + L_z) \frac{d \omega_z}{d t} = M_z - \rho g V z_1 + \sum_{n=1}^N P_n z_{2n} + M_{z1} + M_{z2}.$$

where $d x / d t = v_x$; $d y / d t = v_y$; $d z / d t = v_z$; $d \theta / d t = \omega_x$; $d \psi / d t = \omega_y$; $d \varphi / d t = \omega_z$; m is the vessel mass; x and y are the horizontal movements of the vessel; z is the vertical movement of the vessel; ψ is the vessel trim angle; θ is the vessel heel angle; m_x , m_y and m_z are the attached mass of water; L_x , L_y and L_z are the attached moments of water; ω_x , ω_y and ω_z are the projections of angular velocity on axes Ox , Oy and Oz ; v_x , v_y and v_z are the projections of vessel velocity on similar axes; ρ is the water density; g is the acceleration due to gravity; V is the vessel volumetric displacement; F_g is the vessel gravity

(weight displacement); $\sum_{n=1}^N P_n$ is the total weight of cargo accepted on board; F_{x1} , F_{y1} and F_{z1} are the components of water resistance force to hull movements; M_{x1} , M_{y1} and M_{z1} are the moments of water resistance to hull movements; F_{x2} , F_{y2} and F_{z2} are the components of disturbing force; M_{x2} , M_{y2} and M_{z2} are the moments due to wave action; L_{xx} , L_{yy} and L_{zz} are the central moments of inertia of vessel mass relative to coordinate axes; $x_1 = x_{1c} - x_{1g}$, $y_1 = y_{1c} - y_{1g}$, $z_1 = z_{1c} - z_{1g}$, x_{1c} , y_{1c} and z_{1c} are the coordinates of the vessel's center, x_{1g} , y_{1g} and z_{1g} are the coordinates of the vessel's center of gravity; M_{kr} is the heeling moment of external forces; M_{diff} is the trimming moment of external forces. Integration of the left and right parts of the equations of system (1) over time leads to the following result

$$v_x = \int_0^t \frac{F_{x1} + F_{x2}}{m + m_x} d\tau; \quad \omega_x = \int_0^t \frac{M_{kr} - \rho g V x_1 + \sum_{n=1}^N P_n x_{2n} + M_{x1} + M_{x2}}{L_{xx} + L_x} d\tau;$$

$$v_y = \int_0^t \frac{F_{y1} + F_{y2}}{m + m_y} d\tau; \quad \omega_y = \int_0^t \frac{M_{diff} - \rho g V y_1 + \sum_{n=1}^N P_n y_{2n} + M_{y1} + M_{y2}}{L_{yy} + L_y} d\tau; \quad (2)$$

$$v_z = \int_0^t \frac{\rho g V - F_g - \sum_{n=1}^N P_n + F_{z1} + F_{z2}}{m + m_z} d\tau;$$

The initial values of the coordinates and speeds of movement, as well as the angles of rotation and the corresponding speeds were considered as zero, which can be obtained by choosing the origin. Repeated integration of the equations of system (1) over time allows us to obtain the equations of motion of the vessel in the final form

$$x = \int_0^t (t - \tau) \frac{F_{x1} + F_{x2}}{m + m_x} d\tau; \quad \theta = \int_0^t (t - \tau) \frac{M_{kr} - \rho g V x_1 + \sum_{n=1}^N P_n x_{2n} + M_{x1} + M_{x2}}{L_{xx} + L_x} d\tau;$$

$$y = \int_0^t (t-\tau) \frac{F_{y1} + F_{y2}}{m + m_y} d\tau ; \psi = \int_0^t (t-\tau) \frac{M_{diff} - \rho g V y_1 + \sum_{n=1}^N P_n y_{2n} + M_{y1} + M_{y2}}{L_{yy} + L_y} d\tau ; \quad (3)$$

$$z = \int_0^t (t-\tau) \frac{\rho g V - F_g - \sum_{n=1}^N P_n + F_{z1} + F_{z2}}{m + m_z} d\tau ;$$

$$\phi = \int_0^t (t-\tau) \frac{M_z - \rho g V z_1 + \sum_{n=1}^N P_n z_{2n} + M_{z1} + M_{z2}}{L_{zz} + L_z} d\tau .$$

DISCUSSION

In this section we analyze the equations of motion (3) for different values of considered parameters. Figs. 1 and 2 show dependences of the coordinate z, angles θ and ψ on various parameters. Figs. 3 and 4 show similar dependences of the velocities vx, as well as the frequencies ω_x and ω_y .

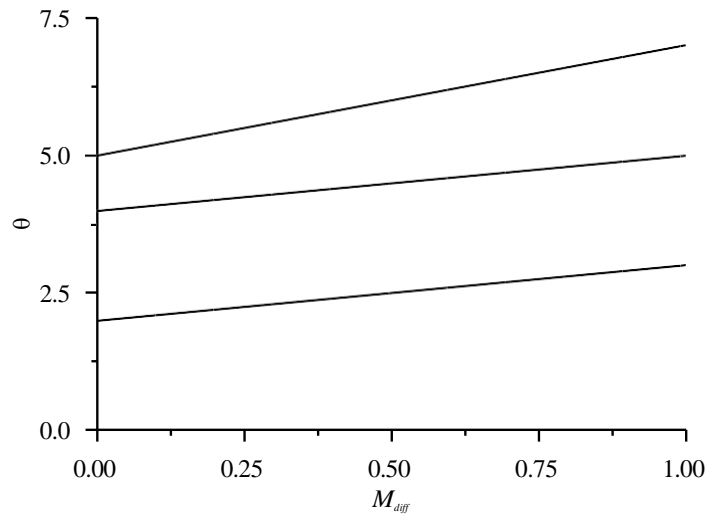


Fig. 1. Typical dependences of the ship's roll angle θ on the heeling moment of external forces M_{kr} . Similar will be the dependences of this angle on the moments M_{x1} and M_{x2} , the weights of the cargo P . The dependences of the z coordinate on the density of water ρ , the acceleration of gravity g , the volumetric displacement of the vessel V , the forces F_{z1} and F_{z2}

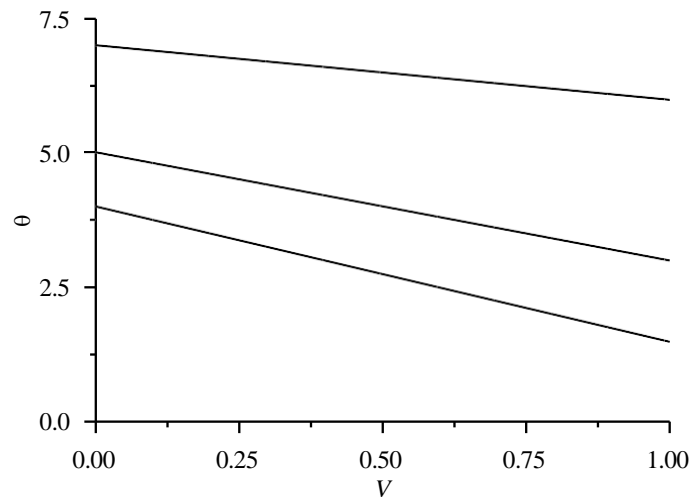


Fig. 2. Typical dependences of the ship's roll angle θ on the volumetric displacement of the ship V . The dependences of this angle on the density of water ρ and the acceleration of gravity g will be similar. The dependences of the z coordinate on the gravity F_g of the weights of the cargo received on the ship P

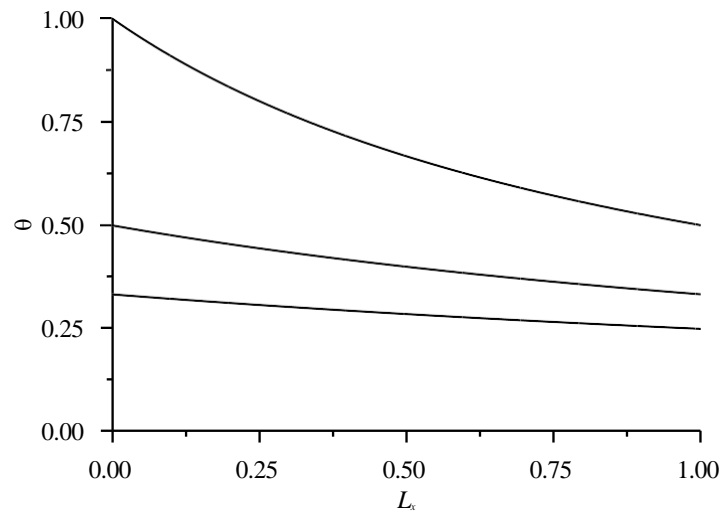


Fig. 3. Typical dependences of the ship's roll angle θ on the central moment of inertia of the ship's mass L_{xx} . The dependence of this angle on the added moments of water L_x will be similar. The dependences of the trim angle of the ship ψ of the same moments will be similar. Also, the dependences of the z coordinate on the masses m and m_z will be similar

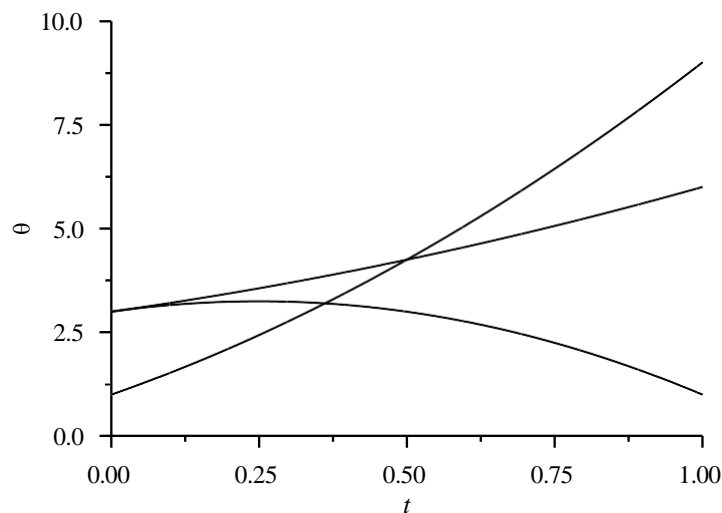


Fig. 4. Typical dependences of the ship's roll angle θ on time t . The time depend-ences of the ship trim angle ψ and the z coordinate are similar

CONCLUSION

We presents a model of vessel motion control with the possibility to change the cargo mass. The model gives a possibility to take into account external forces acting on the vessel, the magnitude of which can be variable. We also present an analytical approach for analysis of the considered model. The approach gives a possibility to take into account changing of parameters of the in time, as well as the nonlinearity of the model.

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